

Viscosity of Mixtures of Liquid Hydrocarbons with Ethene in the Temperature Range 298–453 K at Pressures up to 200 MPa

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The viscosity of mixtures of 2,3,4-trimethylpentane, squalene, 2,2,4-trimethylpentane, 2,2,4,4,6,8,8-heptamethylnonane, polyisobutylene ($M = 500$ g/mol), ethylbenzene, and 1,2-diphenylethane with ethene at elevated pressures was determined with a rolling ball viscometer. Viscosity measurements were made at 298, 353, and 453 K and pressures up to 200 MPa with an accuracy of $\pm 2\%$. The viscosities of the binary mixtures are described as a function of mass fraction and the viscosities of the pure compounds by an empirical equation. The results are compared with literature data of binary nonassociating systems.

Introduction

Experimental viscosities of ethene (1) and of pure hydrocarbons (2, 3) at elevated pressures have been reported previously. This paper extends the investigation to binary mixtures of liquid hydrocarbons with ethene. There are many equations which are able to describe the concentration dependence of the viscosity of nonassociating binary systems, if the viscosities of the pure components are similar. Such models are poor when there are large differences between the viscosities of the pure components. The viscosity results reported here were correlated well by an empirical equation based on the mass fraction and the viscosities of the pure compounds. It is shown that the number of variables influencing the viscosity of binary mixtures of nonassociating compounds can be reduced by the presented method.

Experimental Section

The rolling ball viscometer used for this investigation has been described previously (1, 2).

The liquid hydrocarbons were compressed and fed to the autoclave by a hand pump. At the beginning of a series of measurements the viscometer was calibrated with decane in the total range of temperature and pressure, using the viscosity values of decane published by Naake (3, 4).

After condensing the ethene in a two-stage diaphragm-compressor, it was fed to two high-pressure vessels. The knowledge of the volume and of the pressure dependence of the density (5) made it possible to calculate the pressure difference corresponding to a mass of ethene, so that a known amount of ethene could be metered into the autoclave.

The temperature in the autoclave was measured radially and axially by two NiCr/Ni thermocouples with an accuracy of ± 0.2 K. The pressure could be determined by a calibrated strain gauge pressure sensor with an accuracy of $\pm 0.3\%$. The rolling times were detected inductively and then evaluated by the method of Hubbard and Brown (6). The resulting calibration curves only depended on temperature and pressure.

The scattering of the measured viscosities under constant conditions of temperature, pressure, and concentration was less than $\pm 1\%$. The total uncertainty of the viscosity values was estimated to be $\pm 2\%$ (1, 2), taking into account the accuracy of the literature values used in the calibration. The measurements of mass, volume, and

pressure gave an uncertainty in mass fraction, which was dependent on concentration. The mass fraction (w) has an estimated accuracy between $\pm 1\%$ at $w = 0.8$ and $\pm 3\%$ at $w = 0.2$ (2).

Results and Discussion

The viscosity of the mixtures was determined as a function of temperature, pressure, and concentration. The hydrocarbons measured were 2,3,4-trimethylpentane, squalane, 2,2,4-trimethylpentane, 2,2,4,4,6,8,8-heptamethylnonane, polyisobutylene ($M = 500$ g/mol), ethylbenzene, and 1,2-diphenylethane. The measurements were made at 298, 353, and 453 K and pressures up to 200 MPa with an estimated accuracy of $\pm 2\%$. Approximately 90 measurements for each binary system were made. The viscosity of ethene is reported by Stanislawska and Luft (1). The values of the pure hydrocarbons are reported in refs 2 and 3. The experimental viscosity values of the mixtures of liquid hydrocarbons with ethene are presented in Table 1.

The viscosity of the binary mixtures of decane with methane (4, 7) and decane with carbon dioxide (8) was taken from the literature.

The calculation of the empirical parameters of binary *n*-alkane mixtures was based on the literature values of hexane + dodecane at atmospheric pressure (9–11), as well as of mixtures of hexane and octane with dodecane (12), of hexane + hexadecane (13), and of decane + heptane and decane + hexadecane (14) under pressure. Also the data of binary mixtures of *n*-alkanes with components from octane to pentadecane at atmospheric pressure (15) were used.

The mixtures of *n*-alkanes with aromatic hydrocarbons with dodecane + benzene (11) and binary systems containing toluene or ethylbenzene and *n*-alkanes from octane to hexadecane (16, 17).

The mass fraction dependence of the viscosity for the above systems could be fitted by the equation

$$\ln(\eta/\eta_1) = Aw_2 + \{\ln(\eta_2/\eta_1) - Aw_2\}w_2^B \quad \text{with } \eta_2 > \eta_1 \quad (1)$$

where w_2 is the mass fraction of component 2 (the component with the higher pure-liquid viscosity), η is the viscosity of the binary mixture, and η_1 and η_2 are the viscosities of the pure components 1 and 2.

The empirical parameters A and B were correlated to the logarithm of the relative viscosity of the pure compo-

Table 1 (Continued)

w_2	T/K	P/MPa	$\eta/(mPa\cdot s)$	w_2	T/K	P/MPa	$\eta/(mPa\cdot s)$	w_2	T/K	P/MPa	$\eta/(mPa\cdot s)$
Ethylbenzene + Ethene											
0.7218	298.15	80.0	0.3298	0.8555	298.15	80.0	0.5450	0.9434	298.15	80.0	0.8900
0.7197	298.15	120.0	0.4205	0.8546	298.15	120.0	0.6700	0.9427	298.15	120.0	1.1090
0.7176	298.15	160.0	0.5272	0.8535	298.15	160.0	0.8730	0.9418	298.15	160.0	1.3250
0.7144	298.15	195.0	0.6982	0.8517	298.15	195.0	1.0259	0.9398	298.15	195.0	1.5140
0.7318	353.15	50.0	0.1918	0.8545	353.15	50.0	0.2772	0.9409	353.15	50.0	0.3925
0.7294	353.15	80.0	0.2196	0.8537	353.15	80.0	0.3382	0.9406	353.15	80.0	0.4635
0.7271	353.15	120.0	0.2780	0.8529	353.15	120.0	0.4099	0.9402	353.15	120.0	0.5900
0.7249	353.15	160.0	0.3368	0.8518	353.15	160.0	0.4953	0.9395	353.15	160.0	0.7108
0.7224	353.15	195.0	0.3954	0.8509	353.15	195.0	0.6551	0.9384	353.15	195.0	0.8580
0.7339	453.15	50.0	0.1210	0.8540	453.15	50.0	0.1607	0.9408	453.15	50.0	0.2252
0.7265	453.15	80.0	0.1440	0.8529	453.15	80.0	0.1946	0.9405	453.15	80.0	0.2746
0.7211	453.15	120.0	0.1705	0.8516	453.15	120.0	0.2313	0.9400	453.15	120.0	0.3333
0.7159	453.15	160.0	0.1959	0.8503	453.15	160.0	0.2716	0.9393	453.15	160.0	0.3944
0.7121	453.15	195.0	0.2381	0.8485	453.15	195.0	0.3162	0.9382	453.15	195.0	0.4285
0.8561	298.15	50.0	0.4375	0.9438	298.15	50.0	0.7355				
1,2-Diphenylethane + Ethene											
0.3001	353.15	50.0	0.1166	0.6275	353.15	50.0	0.2534	0.8288	453.15	195.0	0.5997
0.2946	353.15	80.0	0.1406	0.6255	353.15	80.0	0.3060	0.9127	353.15	50.0	0.9602
0.2902	353.15	120.0	0.1680	0.6599	353.15	120.0	0.3838	0.9116	353.15	80.0	1.2040
0.2880	353.15	160.0	0.1981	0.6211	353.15	160.0	0.4728	0.9098	353.15	120.0	1.5824
0.2827	353.15	195.0	0.2304	0.6160	353.15	195.0	0.5633	0.9050	353.15	160.0	2.1057
0.2924	453.15	80.0	0.0946	0.6425	453.15	50.0	0.1537	0.9057	453.15	50.0	0.4186
0.2831	453.15	120.0	0.1177	0.6351	453.15	80.0	0.1867	0.9053	453.15	80.0	0.5097
0.2774	453.15	160.0	0.1388	0.6289	453.15	120.0	0.2341	0.9048	453.15	120.0	0.6336
0.2721	453.15	195.0	0.1523	0.6255	453.15	160.0	0.2848	0.9038	453.15	160.0	0.7633
0.4367	353.15	50.0	0.1584	0.6208	453.15	195.0	0.3340	0.9016	453.15	195.0	0.9093
0.4333	353.15	80.0	0.1891	0.8334	353.15	50.0	0.5531	0.9676	353.15	50.0	1.6718
0.4304	353.15	120.0	0.2304	0.8325	353.15	80.0	0.6710	0.9673	353.15	80.0	2.1196
0.4275	353.15	160.0	0.2782	0.8314	353.15	120.0	0.8559	0.9656	353.15	120.0	2.8663
0.4233	353.15	195.0	0.3387	0.8295	353.15	160.0	1.0784	0.9679	453.15	50.0	0.6028
0.4551	453.15	50.0	0.0982	0.8251	353.15	195.0	1.3409	0.9676	453.15	80.0	0.7504
0.4454	453.15	80.0	0.1215	0.8372	453.15	50.0	0.2741	0.9670	453.15	120.0	0.9516
0.4400	453.15	120.0	0.1502	0.8365	453.15	80.0	0.3367	0.9661	453.15	160.0	1.1559
0.4344	453.15	160.0	0.1792	0.8351	453.15	120.0	0.4199	0.9638	453.15	195.0	1.3762
0.4302	453.15	195.0	0.2088	0.8333	453.15	160.0	0.5075				

nents by polynomials. The parameter B also depends on mass fraction. The resulting equations are

$$A = A_1y + A_2y^2 + A_3y^3 \quad (2)$$

$$B = B_1 + B_2w_2 + B_3y + B_4y^2 \quad (3)$$

where $y = \ln(\eta_2/\eta_1)$.

The average deviation of experimental data was minimized by the simplex method of Nelder and Mead (18). The resulting values of the adjustable parameters are listed in Table 2. Some of the corresponding planes of the logarithm of relative mixture viscosities as a function of mass fraction and the logarithm of relative viscosity of the pure components are shown in Figures 1–3.

In all cases no additive temperature or pressure dependence of the mixture viscosities could be seen. Mixtures with similar components such as the aromatic hydrocarbons ethylbenzene and 1,2-diphenylethane and mixtures with components of the same homologous series like *n*-alkanes or oligomeric isobutenes (2,2,4-trimethylpentane, 2,2,4,4,6,8,8-heptamethylnonane, polyisobutylene ($M = 500$ g/mol)) could be described by the same set of empirical parameters.

The viscosity increases monotonically with increasing relative viscosity of the pure components and with mass fraction of the pure liquid component having the higher viscosity. The logarithmic plot of the relative viscosity of the binary mixtures shows a linear concentration dependence in the range from $w_2 = 0$ to $w_2 = 0.6$. At higher values of w_2 the slope increases with increasing mass fraction. But the slope of the straight lines and the increase with the relative viscosity of the pure components depend on the type of the binary system. Both increase

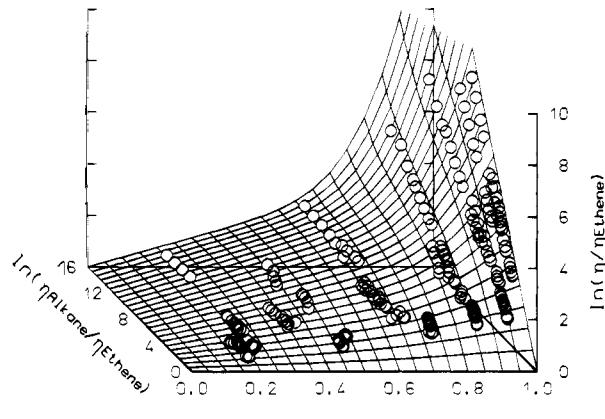


Figure 1. Relative viscosity of mixtures of oligomeric isobutenes (2,2,4-trimethylpentane, 2,2,4,4,6,8,8-heptamethylnonane, polyisobutylene ($M = 500$ g/mol)) with ethene as a function of mass fraction and of the viscosity of the pure components.

starting from mixtures of oligomeric isobutenes with ethene, to squalane + ethene, to binary mixtures of *n*-alkanes and of decane + methane, up to decane + carbon dioxide, which show an almost linear dependence over the whole range of concentration. So, as the relative viscosity of the pure components increases, progressively pronounced differences can be observed between the systems of binary mixtures.

The viscosity values of 2,3,4-trimethylpentane + ethene are similar to those of binary mixtures of *n*-alkanes and can be described by the empirical parameters of *n*-alkane mixtures ($\delta = 0.048$).

The plane of mixtures of oligomeric isobutenes with ethene (Figure 1) is frequently observed in binary mixtures

Table 2. Parameters in the Polynomials 2 and 3 of Eq 1 of the Viscosity of Binary Mixtures

mixture	A_1	A_2	A_3	
oligomeric isobutenes + ethene	0.7177	-0.0407	0.000 66	
2,3,4-trimethylpentane + ethene	-0.2888	0.3237	-0.005 20	
squalane + ethene	0.3668	0.1002	-0.010 39	
aromatic hydrocarbons + ethene	0.5229	-0.1338	0.037 80	
decane + methane	1.4804	-0.4266	0.065 67	
decane + carbon dioxide	0.9102	-0.0469	0.026 14	
<i>n</i> -alkanes + <i>n</i> -alkanes	0.6960	0.1816	-0.083 53	
<i>n</i> -alkanes + aromatic hydrocarbons	-0.7538	0.2866	0.007 00	
mixture	B_1	B_2	B_3	
oligomeric isobutenes + ethene	5.352	-2.967	1.243	
2,3,4-trimethylpentane + ethene	12.622	1.040	-11.324	
squalene + ethene	-9.506	0.780	5.420	
aromatic hydrocarbons + ethene	7.683	2.918	-6.013	
decane + methane	8.209	1.911	1.202	
decane + carbon dioxide	-77.991	10.872	38.135	
<i>n</i> -alkanes + <i>n</i> -alkanes	1.210	2.381	2.398	
<i>n</i> -alkanes + aromatic hydrocarbons	1.404	0.248	-0.836	
mixture	δ^a	y_{\min}	y_{\max}	lit.
oligomeric isobutenes + ethene	0.065	0.0	16.0	2
2,3,4-trimethylpentane + ethene	0.031	1.6	2.8	2
squalane + ethene	0.055	3.0	9.0	2
aromatic hydrocarbons + ethene	0.045	1.5	4.0	2
decane + methane	0.035	2.0	4.5	4, 7
decane + carbon dioxide	0.030	2.2	3.2	8
<i>n</i> -alkanes + <i>n</i> -alkanes	0.010	0.0	3.0	9-15
<i>n</i> -alkanes + aromatic hydrocarbons	0.012	0.0	2.0	11, 16, 17

^a δ = average absolute deviation of experimental values of $\ln(\eta/\eta_1)$. The experimental values are in the range from $\ln(\eta_2/\eta_1) = y_{\min}$ to $\ln(\eta_2/\eta_1) = y_{\max}$.

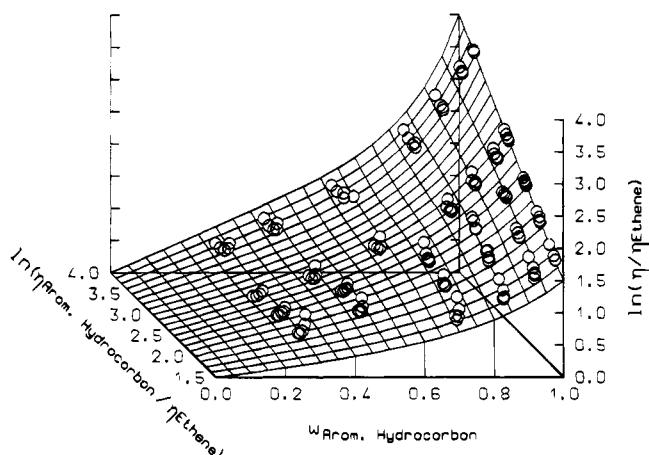


Figure 2. Relative viscosity of mixtures of aromatic hydrocarbons (ethylbenzene, 1,2-diphenylethane) with ethene.

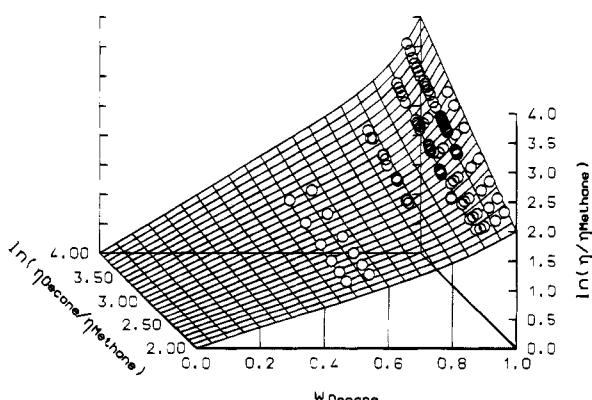


Figure 3. Relative viscosity of decane + methane.

of nonassociating compounds. Examples of binary systems which can be described by the empirical parameters of mixtures of oligomeric isobutenes with ethene (Table 2) are

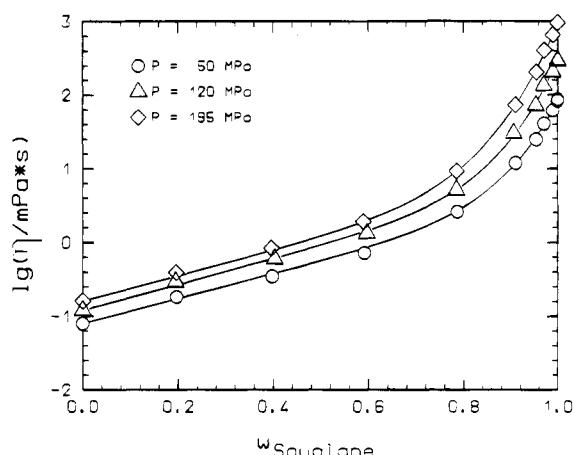


Figure 4. Logarithmic plot of the viscosity of squalane + ethene as a function of mass fraction at 298.15 K.

the mixtures of aromatic hydrocarbons with ethene ($\delta = 0.065$), squalane + ethane (19) ($\delta = 0.053$), mixtures of cyclohexane with hexane (20) ($\delta = 0.023$) and with dodecane (11) ($\delta = 0.011$), and mixtures of *n*-alkanes with aromatic hydrocarbons ($\delta = 0.030$).

The viscosity of pure components can be described as a function of pressure and temperature by empirical equations (1-3). These equations were combined with eq 1. Using the resulting equation and the parameters of Table 2, it is possible to describe the viscosity of the binary systems as a function of pressure, temperature, and mass fraction.

Figures 4 and 5 show some of the calculated curves together with experimental viscosities measured by our group (1-3). Under constant conditions of temperature and pressure the logarithm of the viscosity increases with increasing mass fraction of the hydrocarbon (Figure 4), and the isobars are almost parallel at constant temperature.

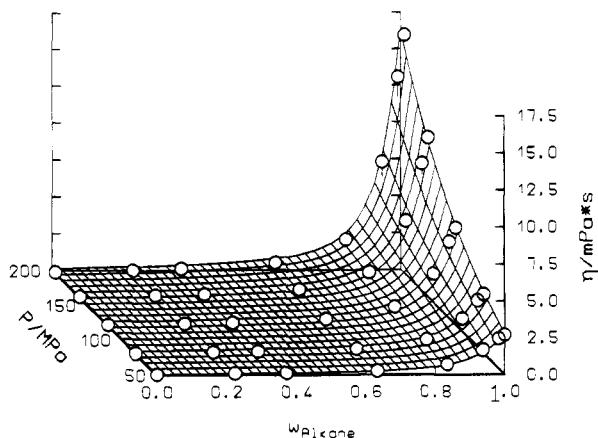


Figure 5. Viscosity of 2,2,4,4,6,8,8-heptamethylnonane + ethene as a function of mass fraction and of pressure at 353.15 K.

Figure 5 illustrates the typical concentration and pressure dependence of the viscosity of hydrocarbon + ethene.

The measured viscosities were also fitted by equations which describe the mixture viscosity as a function of mole fraction (2), like the equation of Grunberg and Nissan (12, 13) or the models of McAllister (21). The best results were obtained with the four-body model of McAllister (21) and with the equation of Soliman (22). In both cases the temperature and pressure dependence of the adjustable parameters could be described by quadratic equations of $\ln(\eta_1 \eta_2)$, where η_1 and η_2 are the kinematic viscosities of the pure components. The number of adjustable parameters was therefore nine for the modified McAllister model and six for the modified equation of Soliman. The deviation of measured viscosities from data calculated by these equations is substantially higher than the deviation from eq 1, which is based on mass fraction.

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